The following tech sheet summarizes the contents of NCMA Test Method SRWU-1 and provides guidelines when interpreting connection strength data for Allan Block Retaining Wall Design. This summary provides the information that is most commonly used, but Allan Block does not claim that all information in the test method is represented in this Tech Sheet.

**TEST OBJECTIVE**

The objective of the NCMA Test Method SRWU-1 “Determination of Connection Strength between Geosynthetics and Segmental Concrete Units” is to define the connection strength between a layer of geosynthetic reinforcement and concrete segmental retaining wall units (SRWs). The result of the test is a linear empirical design equation that is a function of normal load, or the height of the stacked retaining wall units above the connection.

**TEST METHOD & PROCEDURE**

The test method involves building a test specimen that is as close as possible to a replica of a field construction specimen. This includes using full scale SRWs and geosynthetic reinforcement. The SRWs are filled with granular infill and compacted with a vibratory compactor meeting the Allan Block specifications for installation. The minimum width of the SRW specimen is 42in (1060mm) and the minimum width of the geosynthetic specimen is 36in (910mm).

The test specimen is constructed in a frame that will not yield under the stresses of the test. The blocks must be secured in the frame not allowing movement during the test. The frame is designed to be able to apply normal load at a uniform constant pressure with a vertical piston/actuator. A horizontal piston/actuator is used to apply a tensile load to a constant deformation rate. Load cells are used on both the vertical normal load and horizontal tensile load to measure the magnitude of the load throughout the test. Finally two Linear Variable Displacement Transducers (LVDT’s) are used to measure the horizontal displacement of the geogrid during the test.

![Connection Strength Test Frame](image-url)
The test is run numerous times in order to determine the relationship between connection strength or horizontal tensile load and the vertical normal load. The normal load is varied for each different test run generating different connection strengths at failure. Failure is described in two different ways, the Ultimate State and the Service State.

Ultimate State: The ultimate (peak) connection load. The load will occur immediately before the system fails such as the geogrid ruptures, the geosynthetic slips out of the SRWs, the SRWs lifts up or the SRWs fracture.

Service State: The measured connection load at a prescribed deformation criterion. The load occurs when the geogrid has moved relative to the block measured by the LVDT’s. The deformation criteria is established as 0.75 in (19 mm).

In order to ensure the validity of the test one single normal load level is repeated three times. The results of those three repetitions must agree within 10% from the mean of the three tests.

TEST RESULT INTERPRETATION

The results of the connection strength test are linear design equations. They can be compared to the actual tensile load on any given geosynthetic layer to determine the factor of safety for their connection. The equations are a function of normal load. The normal load is based on the height of wall above the connection elevation and the density of the SRWs including the granular infill.

These equations are empirical, based on the best fit line to the data points. Often in order to fit the data accurately a two segment data fit is used. This results in one equation for the lower normal loads and another for the higher normal loads. In design it is required to identify the normal load that separates the two segments. Therefore as many as four equations may describe the ultimate and service state conditions.

Example: Based on Figure 2: determine the Ultimate State Connection Strength for N = 863 lb/ft.

Ultimate State

- \( T_{u1} = 1000 \text{ lb/ft} + N \tan 30^\circ \)
- \( T_{u2} = 1800 \text{ lb/ft} + N \tan 8^\circ \)

Separating Normal Load

- \( 1000 \text{ lb/ft} + N \tan 30^\circ = 1800 \text{ lb/ft} + N \tan 8^\circ \)
- \( N = (1800 \text{ lb/ft} - 1000 \text{ lb/ft})/(\tan 30^\circ - \tan 8^\circ) \quad N = 1831 \text{ lb/ft} \)

Therefore use \( T_{u1} \)

- \( T_{u1} = 1000 \text{ lb/ft} + (863 \text{ lb/ft}) \tan 30^\circ \)
- \( T_{u1} = 1498.3 \text{ lb/ft} \)